

Electro-Thermo-Mechanical Modeling

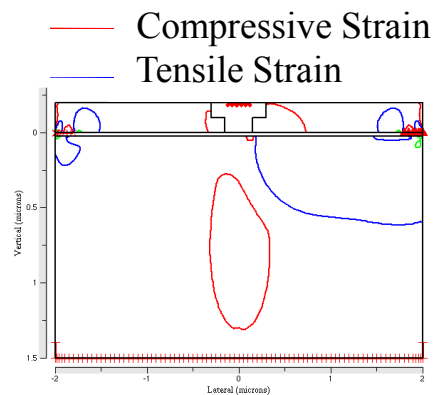
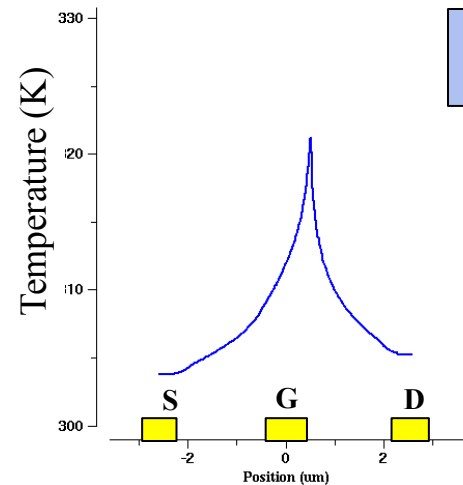
Erin Patrick, Mark Law



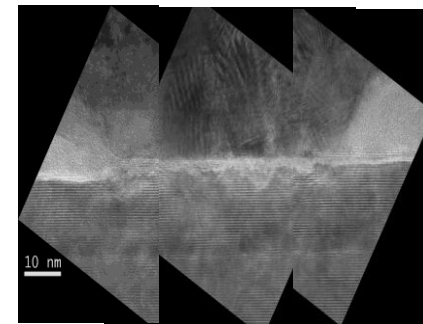
Code Development for Multiphysics Modeling

FLOORS

Electro-Thermo-Mechanical Modeling



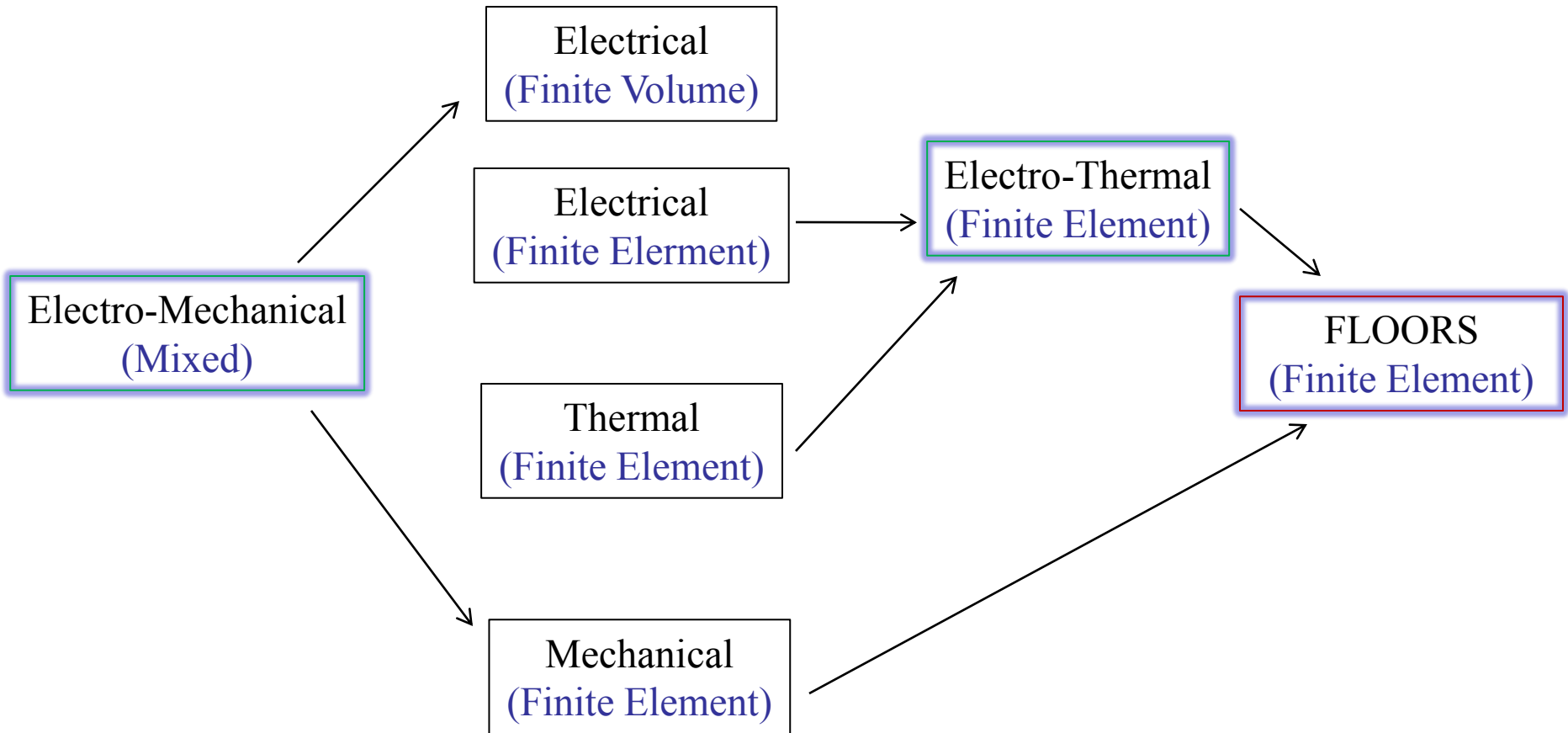
Defect Modeling → Device Performance Prediction



$t=0$, As Built

$t>0$, Degradation

Discretization Methods



Discretization – Current Density

Quasi-Fermi
Current Density

$$J_n = -q\mu_n n \nabla \phi_n$$

$$J_p = -q\mu_p p \nabla \phi_p$$

Boltzmann Relations

$$\phi_n \equiv \psi - \frac{kT}{q} \ln(n / n_i)$$

$$\phi_p \equiv \psi + \frac{kT}{q} \ln(p / n_i)$$

Drift-Diffusion
Current Density

$$J_n = qn\mu_n E + qD_n \nabla n$$

$$J_p = qp\mu_p E - qD_p \nabla p$$

- To obtain a closed system of equations, current densities written as function quasi-Fermi levels
- Using Boltzmann relations, current density can be written in the familiar relationship as the sum of drift and diffusion components
- Drift-Diffusion subtracting large numbers is not a good recipe with finite precision arithmetic

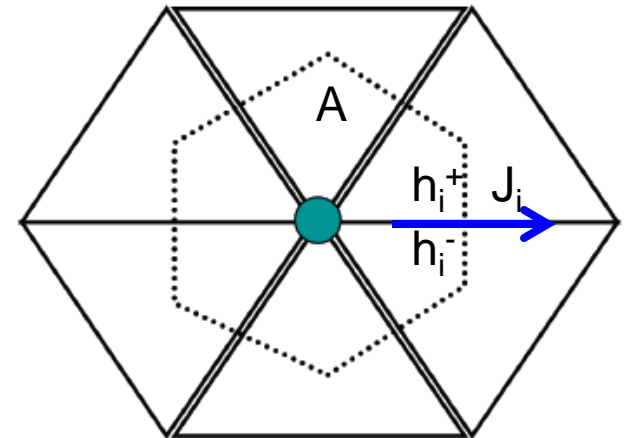
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Finite Volume Scharfetter-Gummel (FVSG)

- Each PDE is integrated over a control volume A
- A is defined by the perpendicular bisectors of mesh elements
- PDE integrated using Green's formula
- Current $J_{n,p}$ evaluated using the Scharfetter-Gummel
- Scharfetter Gummel
 - Assume field and current constant
 - Solve resulting equation
 - $J_n/q = D (B(t) n_{i+} - B(-t) n_{i-}) / l_i$
 - $t = \mu E / D$
 - $B(t) = t / (e^t - 1)$ Bernoulli Function
- Advantages:
 - Commonly used “proven” method
 - Assembly time, each edge assembled once
- Disadvantages
 - Current defined only on edges, not continuous in space
 - Impact Ionization, Joule Heating more difficult
 - Works best when grid is aligned with current flow

$$\mathbf{J}_n = qn\mu_n \mathbf{E} + qD_n \nabla n$$

$$\frac{dn}{dt} = \frac{1}{q} \nabla \cdot \mathbf{J}_n - U_n$$



$$\frac{1}{q} \sum_i J_i (h_i^+ + h_i^-) - A \left(U_n + \frac{dn}{dt} \right) = 0$$

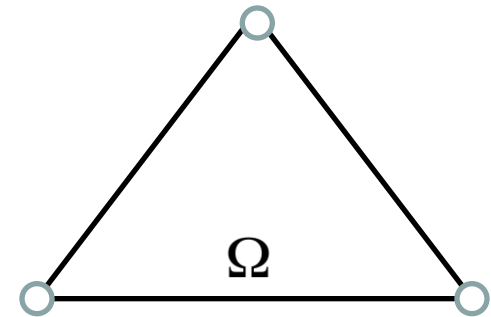
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Finite Element Quasi-Fermi (FEQF)

- $\phi_{n,p}$ defined at grid nodes
- Use shape function in an element
 - Piecewise linear most common
 - Can be higher order
- Integrate equations and minimize error
- Advantages:
 - Current is a continuous function over each element
 - Easier to compute Joule Heating, Impact Ionization
 - Compatible with strain calculations
- Disadvantages
 - Not as stable
 - Convergence issues

$$\mathbf{J}_n = -q\mu_n n \nabla \varphi_n$$

$$\frac{dn}{dt} = \frac{1}{q} \nabla \cdot \mathbf{J}_n - U_n$$



$$a(\psi, v) \equiv (-\rho, v)$$

$$a(\psi, v) \equiv \iint_{\Omega} \epsilon \nabla \psi \cdot \nabla v \, dx \, dy$$

$$(-\rho, v) \equiv -\iint_{\Omega} \rho v \, dx \, dy$$

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Electro-Thermo-Mechanical Simulation

Electro:

Poisson's Eq.

$$\nabla^2 \Psi = -\frac{q}{\epsilon} (p - n + N_D - N_A)$$

Electron/Hole Continuity Eq.

$$\frac{dn}{dt} = \frac{1}{q} \nabla \cdot \mathbf{J}_n$$

$$\mathbf{J}_n = -q\mu_n n \nabla \phi_n$$

Thermo:

Heat Eq.

$$c \frac{\partial T}{\partial t} - \nabla \cdot K \nabla T = Q \quad \text{where,}$$

$$Q = \mathbf{J}_n^2 \frac{1}{q\mu_n n}$$

Mechanical:

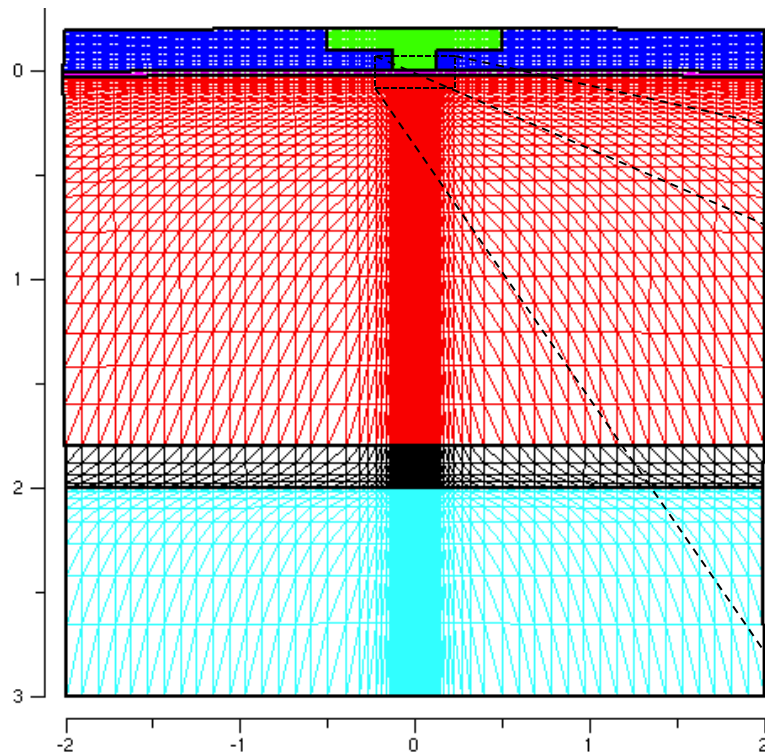
Equilibrium Eq.

$$\nabla \cdot \sigma + F = \rho \nabla^2 u \quad \text{where,}$$

$$\sigma = D (\epsilon - \epsilon_0) \quad D(T) \text{ function of temperature}$$

$$\epsilon = \nabla \Psi \cdot d_{pz}$$

Simulation Results on GaN hemt - Baseline

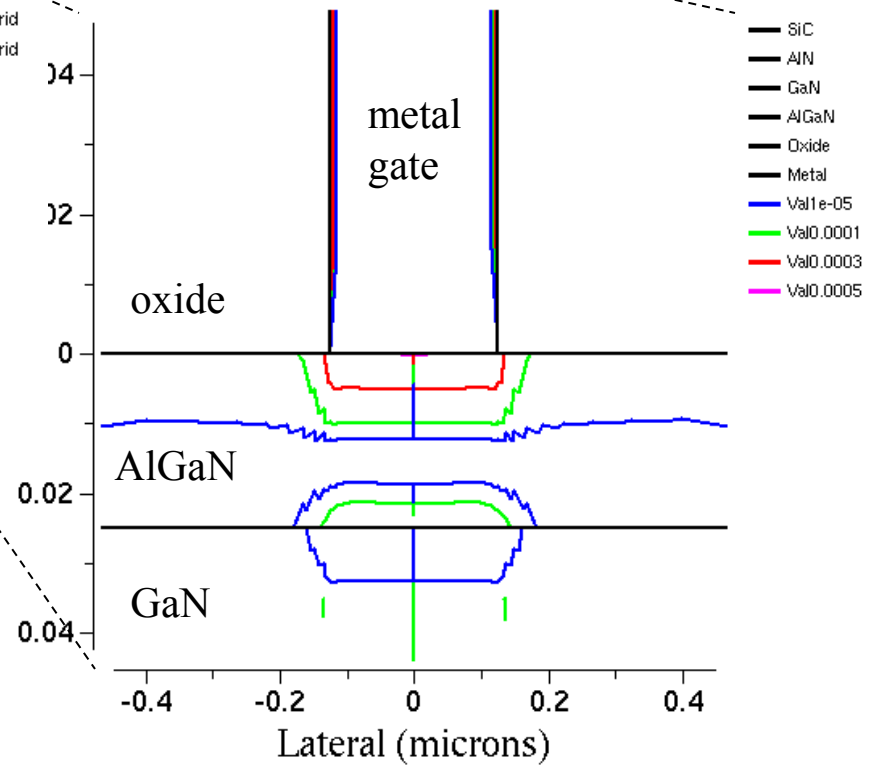


$$V_{gs} = 0 \text{ V}$$

$$V_{ds} = 0 \text{ V}$$

$$T = 300 \text{ K}$$

Tensile Strain Contours



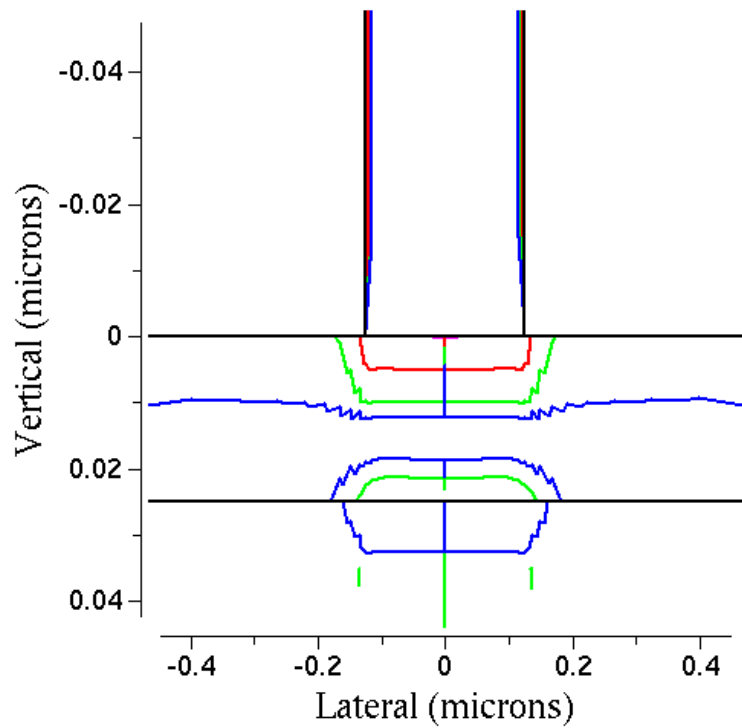
Inverse Piezoelectric Effect

No temperature dependence
on Young's modulus

$$V_{gs} = 0 \text{ V}$$

$$V_{ds} = 0 \text{ V}$$

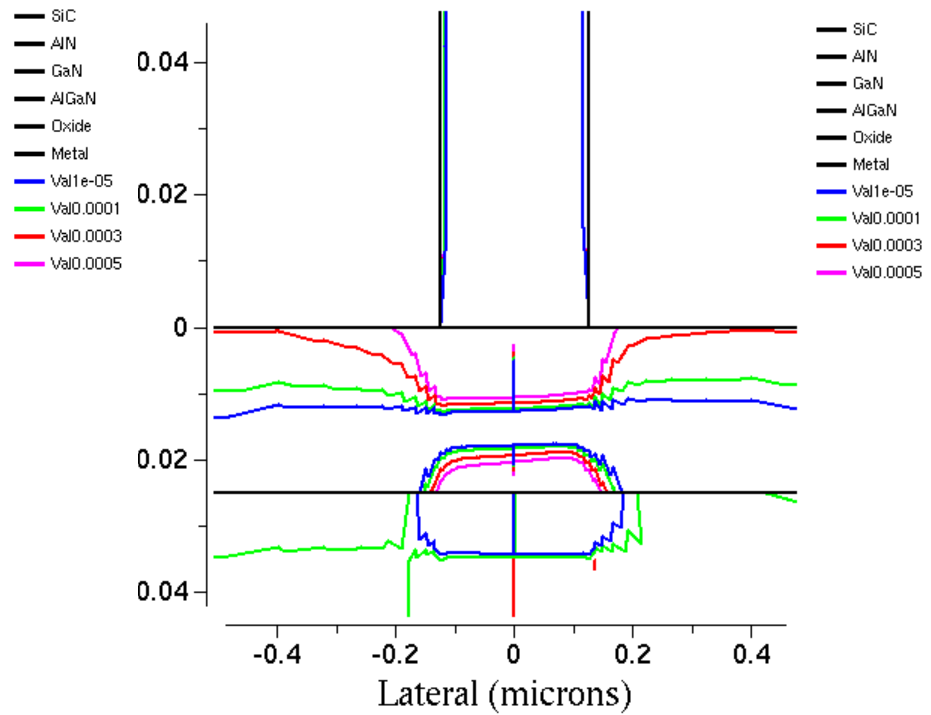
$$T = 300 \text{ K}$$



$$V_{gs} = 0 \text{ V}$$

$$V_{ds} = 6.1 \text{ V}$$

$$T(\text{max}) = 500 \text{ K}$$

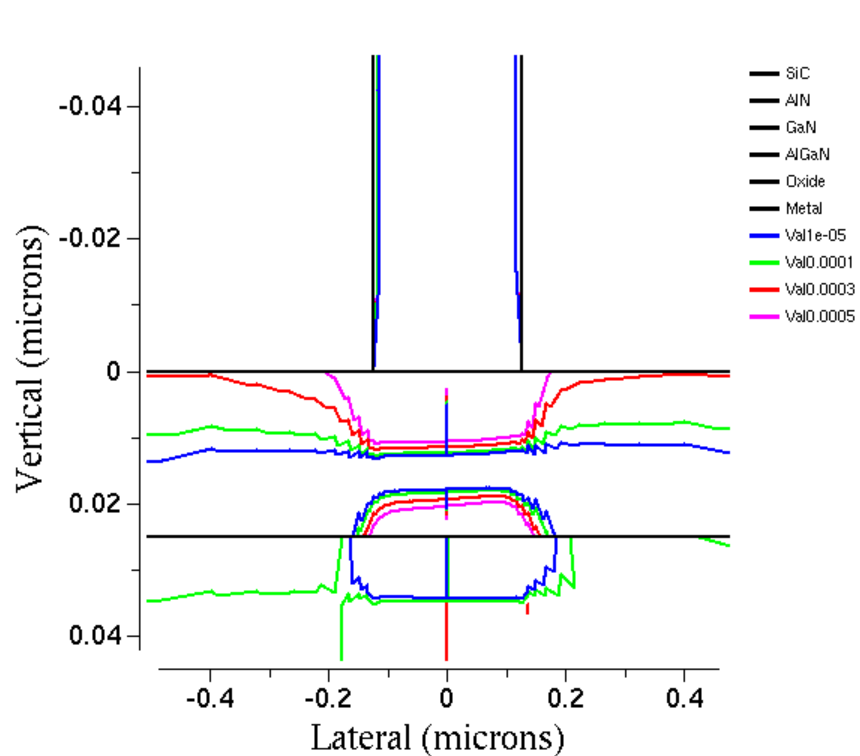


Temp dependence on Young's Mod.

No temperature dependence
on Young's modulus

$V_{gs} = 0 \text{ V}$ $V_{ds} = 6.1 \text{ V}$

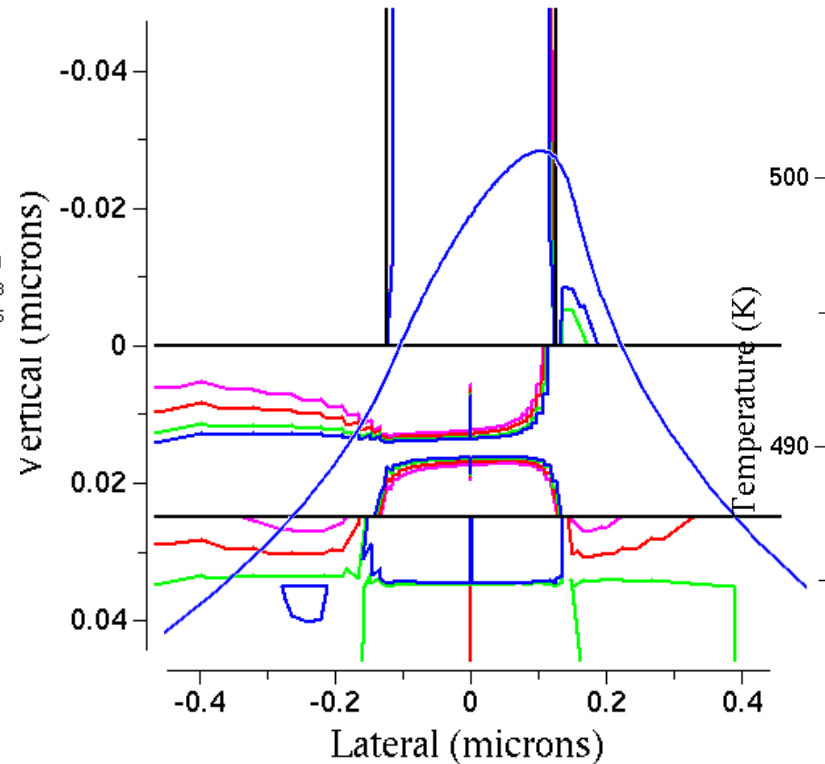
$T(\text{max}) = 500 \text{ K}$



Temperature dependence
on Young's modulus

$V_{gs} = 0 \text{ V}$ $V_{ds} = 6.1 \text{ V}$

$T(\text{max}) = 500 \text{ K}$



Summary and Future Work

- A finite element based simulator is needed for the the full electro-thermo-mechanical model
 - Couples mechanical strain with Joule heating and electrical operation
- Future Work
 - Incorporate David's work on Electromechanical degradation
 - Collaborate with Dr. Nishida's group to develop a model for gate leakage current